

RESEARCHES REGARDING THE ELABORATION OF THE COMPOSITE MICROPOWDERS WITH WOLFRAM MATRIX USING MECHANICAL ALLOYING TECHNIQUE

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ABSTRACT

The main purpose of this paper is to presents some researches regarding the composite micropowders with wolfram matrix in mixture with copper used in production of the electrical contacts. In order to alloy the two powder, the mechanical alloying is used. The SEM micrograph of the tungsten micropowder and copper and then the SEM micrograph of the mixture WC-Cu for the different mechanical alloying time are presented.

Keywords: Micropowders, copper, mechanically alloyed, SEM micrograph

1. INTRODUCTION

Copper alloys are one of the most commonly used materials for various engineering applications, although one of the factors limiting the wider application of copper and copper alloys is from the one hand relatively low mechanical strength and on the other hand the large density. Silicon carbide (SiC) is recognized as one of the potential candidates for electronic packaging and thermal management applications. Metal matrix composite materials reinforcement by Al_2O_3 were developed by various methods and also found wide application where the high electrical conductivity, high thermal conductivity and high strength and low wear resistance are required

Composite material WC/Cu is applied as the electrical contacts, resistance welding electrodes and electrodes for automatic welding.

One of the most technique to alloy the WC powder an Cu powder is mechanical alloying, a recent technique used for this materials, [1], [5].

Copper tungsten sintered materials are manufactured with different copper contents, from 20% up to 70%, depending on the use to which they are put, [3]. The method of manufacture depends on the percentage of tungsten present. Materials with large

percentages of tungsten (around 80%) are generally made by the impregnation process, where it is advantageous to use a coarse grain tungsten powder to decrease arc erosion.

For percentages of the order of 60%, liquid phase sintering is more appropriate, and for materials with less tungsten, powder mixtures without a liquid phase are sintered together.

Materials with a low copper content are used for high currents to improve contact life and breaking capacity. With a higher copper content, about 67%, the material erodes slightly less than pure copper, at low currents (around 20 amp), and the improvement in erosion resistance is enhanced at higher currents, but this is accompanied by considerable deformation of the contact surface. The contact resistance increases considerably on arcing, due to oxidation and depletion of copper in the interface.

The lack of solubility of W in Cu makes W-Cu a model system for liquid phase sintering because densification can be attribute to either particle rearrangement or solidstate sintering of the skeletal structure, [7].

The final shape and, also, the physical and mechanical characteristics of the micropowders are obtained through the microwave technique, the known as a very useful technique for this type of refractory materials, [2], [6].

2.2. POWDER CHARACTERISTICS

2.1. Copper powder

In order to elaboration the composites materials with tungsten micropowder matrix and copper for electrical contacts the next powder type was used (tables 1 and 2 for copper powder and tables 3 and 4 for tungsten powder). The copper powder was SEM characterization using an electronic microscope, FEI -INSPECT from INFLPR Bucharest, and are presented in Figs. 1, 2, 3 and 4. Due to the electrolytic process, the shape of copper powder can be characterized as dendrite.

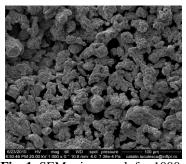
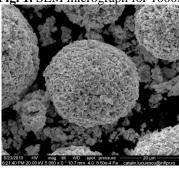


Fig. 1. SEM micrograph for 1000x



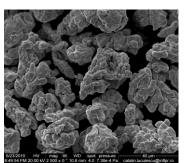


Fig. 2. SEM micrograph for 2500x

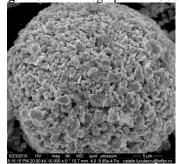


Fig. 3. SEM micrograph for 5000x 2.2. *Tungsten powder*

Fig. 4. SEM micrograph for 10000x

In this paper K30 powder type was used with the chemical composition presented in table 3, and SEM micrograph for different magnification in figs. 5 to 8.

Table 1. The main characteristics of the copper powder

Powder	Density at	Atomic	Thermal	Fusion	Brinell
	20 °C	volume	conductivity	point	Hardness
	[g/cm³]	[cm³/atg]	[cal/cm°CS]	[°C]	[daN/mm²]
Cu	8.92	10.28	1	960	35

Table 2. Physical and chemical characteristics of the Pcu99 copper powder type

Powder	Type	Purity [%]	Purity [%]	Apparent density [g/cm ²]	Grain maximum dimension [μm]
Cu	Pcu99	99.50	99.50	1.0 - 1.2	5

Table 3. Chemical composition of the K30 powder type [%]

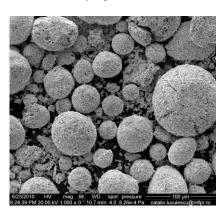
Group ISO	WC	TiC	TaC	CO	C total
K30	90.3	0.2	0.5	8.7-9.3	5.62-5.7-5.78

3. MECHANICAL ALLOYING

In order to elaborate the tungsten nanopowders a mechanical alloying technique and Pulverisette 6 vario-planetary ball mill were used.

The working process parameter was:

- bowl volume: 250 ml;
- bowl material: stainless steel;
- ball diameter: Φ=10 mm;
- balls number: 50 pieces;
- balls material: stainless steel;
- material/ball ratio: ½ (100gs powder K30+Cu and 200 gs, balls);
- alloying environment: air
- alloying times: 5, 10, 15 hours



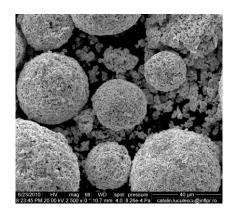




Fig. 7. SEM micrograph for 5000x

Fig. 6. SEM micrograph for 2500x

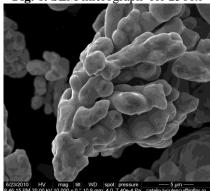


Fig. 8. SEM micrograph for 10000x

Table 4. The concentration of copper and tungsten powders for mechanical alloying

Samples	Cu, [%]	K30, [%]
1.	35	65
2.	30	70
3.	25	75

Table 4 shows the concentration of copper and tungsten powders for mechanical alloying. In order to mechanical alloying nine samples was prepared:

3 samples K30 (65%)-Cu(35%), using three time for mechanical alloying: 5,10 and 15 hours;

3 samples K30 (70%)-Cu(30%), using three time for mechanical alloying: 5,10 and 15 hours;

3 samples K30 (75%)-Cu (25%), using three times for mechanical alloying: 5, 10 and 15 hours.

The ratio of mixture was done using a precision analytical balance WPS 510. The weigh of each sample is 100 gs.

4. CHARACTERISATION OF POWDER MIXTURES

The mixture **K30/Cu** with the ratio **65/35** is presented in Figs 9 to 11.

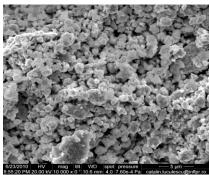


Fig. 9. SEM micrograph of the mixture K30 (65)–Cu(35) alloying time: 5 hours;

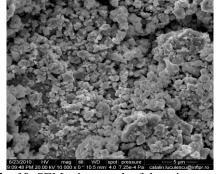


Fig. 10. SEM micrograph of the mixture K30 (65)–Cu (35) alloying time: 10 hours;

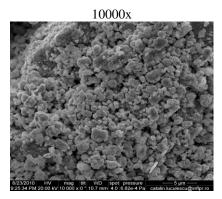


Fig. 11. SEM micrograph of the mixture K30 (65)–Cu (35) alloying time: 15 hours; 10000x

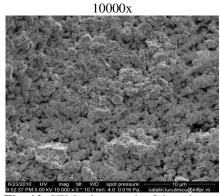


Fig. 12. SEM micrograph of the mixture K30 (70) – Cu (30) alloying time: 5 hours; 10000x

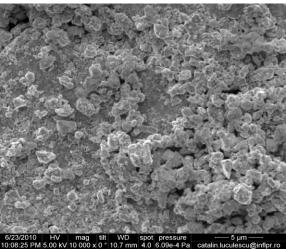


Fig. 13. SEM micrograph of the mixture K30 (70)–Cu(30) alloying time: 10 hours; 10000x

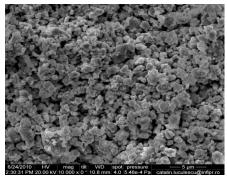


Fig. 14. SEM micrograph of the mixture K30 (75)–Cu (25) alloying time: 5 hours; 10000x

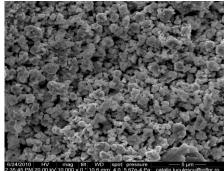


Fig. 15. SEM micrograph of the mixture K30 (75)–Cu (25) alloying time: 10 hours; 10000x

The mixture **K30/Cu** with the ratio **70/30** is presented in Figs 12 to 13. The mixture **K30/Cu** with the ratio **75/25** is presented in Figs 14 to 15.

5. CONCLUSIONS

In order to elaborate the W - Cu nanostructured powders the mechanical alloying technique was used;

From SEM analysis it is observed that the particles are agglomerated specially at higher times of mechanical alloying. There are the difference between copper particles and tungsten particles;

The shape for all the three samples obtained after 8 hours of mechanical alloying by friction mode respectively shock mode is irregular.

REFERENCES

- 1. **Bothate A.A.**, Advances in W-Cu: New powder systems, PhD Thesis, San Diego State University, 2000.
- 2. **Mondal A., Agrawal D., Upadhyaya A.**, Microwave Sintering of Refractory, Metals/alloys: W, Mo, Re, W-Cu, W-Ni-Cu and W-Ni-Fe Alloys, *Journal of Microwave Power and Electromagnetic Energy*, 44 (1), 2010, pp. 28-44.
- 3. *** Copper in Electrical Contacts, Technical Note 23, 1980, *Copper Development Association*, Publication 23, July 1997, pp. 1-21.
- 4. **Teisanu C., Gheorghe St., Ciupitu I.,** Sintering temperature influence on physical characteristics of the sintered Iron-Copper based alloy, *Sintering '05*, Grenoble, August 29-September 1, 2005, pp. 507-510
- 5. **Nicolicescu** C., Cercetări privind elaborarea și caracterizarea contactelor electrice nanostructurate pentru curenți de mare putere (in Romanian), PhD Thesis, 2009.
- 6. **Gingu O., ş.a.,** Processing of PM composites materials by microwave sintering, *Sintering '05*, Grenoble, August 29-September 1, 2005, pp. 139-142.
- 7. **Johnson J.L., German R.M.,** Densification and distorsion of liquid phase sintered W-Cu, *Sintering* 05, Grenoble, August 29-September 1, 2005, pp. 291-294.